Best Practices for Evaluating the Capability of Nondestructive Evaluation (NDE) and Structural Health Monitoring (SHM) Techniques for Damage Characterization

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- Process for evaluating NDE 'sizing' capability
- Emphasize *understanding assumptions* in evaluation
- Challenges with SHM Capability Evaluation
- Best Practices from Demonstration Study
- Opportunities for Models in Evaluation (MAPOD)

Drivers for Damage Characterization in Aircraft Structures

Opportunities for Accurate Characterization Techniques:

- Need for small crack size 'binning'
 - Better guide *maintenance actions*
- Fatigue crack parametric characterization (sizing, localization) using eddy current NDE
 - Significant opportunity for support of condition-based maintenance (CBM)
- Complete crack characterization evaluation (*multiple cracks* at single site)
 - Provide better data for life prediction models
 - Supports digital twin concept

Validation Procedures are Needed to Ensure Accurate Characterization and Localization Techniques



layers

Quality Metrics for Damage Localization / Characterization

Review of Evaluation Methods (Metrics) for Characterization:

• 1) Statistics Community:

- A) Measurement System Analysis (MSA), ANOVA Gauge R&R (Repeatability and Reproducibility)
 - ASTM E2782 Standard Guide for Measurement Systems Analysis
 - NIST: Guide to the Expression of Uncertainty in Measurement

 $y = f(x_1, x_2, ..., x_n)$ where:

$$\sigma_{y} \approx \sqrt{\sum_{i=1}^{n} \left(\frac{\partial f}{\partial x_{i}} \sigma_{x_{i}}\right)^{2}}$$

- y: measurement
 - *f*: measurement model
 - *x*: uncertainty components (*n*)
- Brown, J., ASNT Fall Conference, 2011
- Issues:
 - Conventional analysis approaches (ANOVA) don't naturally address <u>complex models</u> with multiple parameters
 - Uncertainty propagation often assume 'independent parameters'; They typically do not address joint probability (covariance)
 - Need to address <u>aleatory and epistemic uncertainty</u> in evaluation
 - These approaches are solely dependent upon <u>raw data</u>.

1. Capability Evaluation and Metrics for Damage Localization / Characterization

Review of Evaluation Methods (Metrics) for Characterization:

• 1) 'Statistics' Community:

• 95% Limit Against Undersizing: $H_{95} = Average(H_i) - 1.64*RMS(H_i)$



Nordtest. 1998. *Guidelines for NDE Reliability and Descriptions, NT Techn Report* 394. 1998.

* Figure from: Ducharme et al., "Automated ultrasonic phased array inspection of fatigue sensitive riser girth welds with a weld overlay layer of corrosive resistant alloy (CRA)" (2012).

Figure 5: Comparison between AUT assessments and DT measurements

(—— Ideal sizing; - - - +/- 0.5 mm; — — +/- 1 mm; ____ Safety limit against undersizing; □ Surface flaw scatter; ◆ Embedded flaw scatter)

* http://www.ndt.net/article/ndtnet/2012/1_Ducharme.pdf

Why a single number summary, a_{90/95}, is an incomplete NDE summary [Annis]



Size, a (mils)

Quality Metrics for Damage Localization / Characterization

Review of Evaluation Methods (Metrics) for Characterization:

- 2) Parameter Estimation / Inversion Community:
 - Estimation Metrics (e.g. CRLB)
 - Knopp et al, 2008, "Estimation Theory Metrics in Electromagnetic NDE"
 - Issue: These metrics are often purely model-based. Do not naturally address parameters/conditions not well-defined by models.
- 3) Uncertainty Quantification Community (Models, MAPOD)
 - Verification & Validation (Emphasis on Scientific Computing)
 - Stochastic Numerical Methods (e.g. Polynomial Chaos)
 - Bayesian Calibration
 - SIAM UQ12
 - Error Estimate with Uncertainty Bounds
 - Challenge: Quality metric is an evaluation of error with *uncertainty bounds* given the full application context (experiment + simulation)
- 4) Foundations for Quality Metrics for NDE/SHM Characterization:
 - Sensitivity Analysis in Inverse Methods [Aldrin et al, 2009]
 - MAPOD for SHM / Radiance Program [Aldrin et al, 2009-2011]

Compare NDE 'Ahat-vs-a' POD and NDE Characterization Error (CE) Evaluations

Ahat-vs-A POD Analysis:

- Follow MIL-HDBK 1823A
- Perform evaluation studies
 - experimental measurements
 - *simulated* measurements
- Evaluate model of measurement (â_i) with respect to flaw size (a_k)
 - *mean* model
 - confidence (uncert.) bounds



Characterization Error Analysis:

- Build on Protocol for NDE/SHM
- Perform evaluation studies
 - experimental *sizing results*
 - simulated sizing results
- Evaluate *characterization error* (ê_j) with respect to flaw size (a_k)
 - error model ($\hat{e}_j = \hat{a}_j a_j$)
 - uncertainty bounds



Compare NDE 'Ahat-vs-a' POD and NDE Characterization Error (CE) Evaluations

Ahat-vs-A POD Analysis:

- Follow MIL-HDBK 1823A
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 - *mean* model
 - *confidence* (uncert.) bounds

Characterization Error (CE) Evaluation is Similar to Ahat-vs-A POD Assessment

Differences:

- Complex multi-dimensional error model
- Simulating 'characterization' more complicated than NDE measurements (MAPOD) a₁

Characterization Error Analysis:

- Build on Protocol for NDE/SHM
- Perform evaluation studies
 - experimental sizing results
 - *simulated* sizing results
- Evaluate *characterization error* (ê_j) with respect to flaw size (a_k)
 - error model ($\hat{e}_j = \hat{a}_j a_j$)
 - uncertainty bounds



What's Missing in NDE Capability Evaluation? [Annis et al., Mat Eval. 2015]

Understand implicit statistical assumptions in regression analysis:

- 1. The model must look like the data!
- 2. The response must be continuous and observable.
- 3. The model must be linear in the parameters.
- 4. The variance must be homoscedastic (uniform variance)
- 5. The observations must be uncorrelated:
 - with respect to time
 - with respect to space
- 6. The errors must be Normal

(global strength of the stren

Target size, a, or log(a)

Target size, a, or log(a)

Replacing censored values with the censoring value skews the result anticonservatively.

If assumptions are not met, you need to pick a different 'correct' model!

"Simply not understanding the nature of the assumptions being made does not mean that they do not exist." Frank et al (1993).

Case Study - Model-based Inversion of EM Signals for Crack Characterization [Shell et al., QNDE 2014]



Developing Characterization Error Models for Inversion Performance [QNDE 2013]

Group Characterization Error Samples into Unique Data Classes:

- 1. P(good classification: with some error)
 - associated with linear ahat-vs-a model
- 2. P(poor classification: due to weak signals)
 - correlated with *small flaw geometry*
 - associated with left 'censoring' in POD
- 3. P(poor classification: due to saturated signals)
 - poor classification, signals smaller than true value
 - associated with right 'censoring' in POD



- observed as 'clusters' at specific parameter estimate plane bounds
- analogous with 'censoring' in POD
- 5. P(poor classification: problem ill-posed / solution stuck in local minima)
 - secondary 'clusters' in error plane
 - need for more complex POD models (mixture models, higher order)
- 6. P(poor classification: due to poor NDE technique)
 - complete failure in sizing procedure
 - result independent of flaw parameters
 - associated with 'random missed call rate' in POD



Developing Characterization Error Models for Inversion Performance [QNDE 2014]

(c)

200



Censoring / constraints

CE, length (mils)

0

-5

-10

-15

0

50

100

length, known (mils)

150

- Interactions and mixture models
- Random missed classifications
- B. Critical to Check Assumptions in Characterization (Statistical) Model



confidence //

Define

limits of

model fits

Consider

clear

error

bound in fit FIGURE 4. (a) RMS of characterization error for three crack dimensions with respect to varying estimated cross-sectional area of crack. Characterization error for censored inversion results for (b) crack depth, (c) crack length and (d) crack width. Plots include a linear model fit (solid line) with confidence bounds (dashed line) and corresponding prediction bounds (dash-dot line).

Verification and Validation of Structural Damage Sensing Systems



- Structural Damage Sensing is a component of SHM
- SDS System Certification <u>requires</u> Qualification Testing that includes Capability (Reliability) Validation
- Structural Damage Sensing (SDS) Reasoner Structural Health Assessment
- SDS System Verification and Validation:
 - Verification: Demonstrate design requirements under controlled conditions (laboratory environment)
 - Validation: Demonstrate design requirements with representative operational environment and user
- Required capability depends on expected application
- Validating SDS capability is a requirement for use of SHM in USAF structures managed via Aircraft Structural Integrity Programs (ASIP)





Protocol comprises:

- Procedure for analyzing all pertinent characteristics of the SDS system
 - Identify all **critical factors** that affect system performance

- Multistage approach for system validation

- Modeling and experimental methodology for efficiently addressing a wide range of damage and operational conditions
- Effective methods for evaluating metrics of capability and reliability depending on system type and function (*uncertainty propagation*)



Primary Protocol



Analyzing Pertinent Characteristics of an SDS System





Model Assisted Probability of Detection (MAPOD)



Model Assisted POD (MAPOD) method:

- Uses models to *minimize* the need for empirical samples to evaluate POD and False Call (FC) rate
- Consensus protocol developed by international working group [2003-11]
 - Transfer function (XF) and full model-assisted [Thompson, 2001]



- Protocol added to MIL-HDBK-1823A
 (2009), Appendix H. See also <u>www.cnde.iastate.edu/MAPOD/</u>.
- Feasibility of approach demonstrated for a number of ultrasonic and eddy current inspection demonstrations:
 - MAPOD/WG Demonstrations [Forsyth, 2008]: XF and FMA¹ examples
 - PICASSO EU project: Several successful POD validation cases

^{1.} J.C. Aldrin, J. S. Knopp, E. A. Lindgren, K. V. Jata, "Model-assisted Probability of Detection (MAPOD) Evaluation for Eddy Current Inspection of Fastener Sites", Review of Progress in QNDE, (to be published, 2009).



Demonstration Study – Define SHM System



SDS System Characteristics:

- **Type:** Direct damage detection using active sensing
- SHM System Output: Damage detection call
- Coverage and Sensor Location: Semi-global (sub-structure)
- Measurement Type: Vibration (low frequency) response
- **Time of Data Acquisition (DAQ):** While aircraft is on the ground
 - Vary temperature (gradients), loading/unloading, boundary cond., fastener torques
- Location of DAQ Hardware: Onboard the aircraft

Structure Characteristics: Include joints in test article

- Center joint with sites for simulating damage growth
- End conditions with optional shims (to change boundary)

Damage Characteristics:



- Damage Types (Failure Conditions) to Detect: (Large) fatigue cracks
 - Approximate crack growth by cutting notches
 - Fastener removal necessary for growing flaw (must maintain equal torque, verify damage metric change not due to changes in boundary conditions)



Simulated Sensitivity Analysis for Representative Low Frequency Global Vibration-based Damage Sensing



Parametric Study

- Frequency
- Source Excitation
 - location
 - orientation
 - distribution
- Sensor(s)
 - location
 - orientation
 - measurements
- Crack (notch) length
- Temperature (elastic property variation)
- Boundary conditions
 - Fastener stiffness
 - Fastener contact
 - End stiffness
- Detection algorithms / metrics
- Characterization algorithms / metrics







Determine Output Variance on Damage Measures (POD) Given Uncontrolled Environmental Variables and Uncertainty

Input Parameters with Variation

- Temperature : (elastic property variation)
- Boundary condition: Fastener stiffness



Output Results

• Damage metric 'distributions' as a function of transducer location and crack length







Input Parameters with Variation

- Temperature : (elastic property variation)
- Boundary condition: Fastener stiffness



Output Results

 POD for varying transducer location and crack length



Demonstration Study – **Identify and Evaluate Controlling Factors**

Sub-tasks



Primary Protocol



Evaluate Controlling Factors – Temperature Variation and Gradients



Temperature Study: Test article placed in Thermotron temperature chamber

- Temperature testing performed from -20°F to 150°F
- Temperature compensation algorithms are necessary for damage metric
- Significant temperature gradients also observed during study
 - Some gradients considered extreme (>45°F) due to end ' thermal sinks'
 - Need to make estimate of expected gradients 'in the field' (10-20°F ?)





Issue 1: Varying shift wrt frequency in FRFs with temperature changes Fit nonlinear model with bias and slope corrections: $f_{new}(f) = f + \left(\frac{\phi_1}{1000 \text{ Hz}}\right) f + \phi_0$



Issue 2: Temperature variation also produces shape changes in FRFs
 ➢ Use three references (FRFs) addressing different temperature bands
 Study: Vary Temperature - Up to 112°F, Down to 32°F, Return to 75°F



Evaluate Controlling Factors – Bond Quality and Sensor Performance



Observations:

- Several accelerometer bonds failed during temperature testing
- Failure was observed at prolonged exposure to 150°F
- Coherence measures can be used to track sensor failure (example below)
 - Differences were observed with sensor 'in partial contact' and 'in air'
- One of the sensor failures was the reference accelerometer (#1)
- Losing the reference sensor is especially detrimental to performance of vibration-based SDS system (FRF)
- SHM computer algorithms need to detect failures and schedule repairs
- Validation studies should include bond failure and repair as varying condition





Evaluate Controlling Factors – Sensitivity to Damage



Observations:

- Damage grown at 1/16" increments up to 0.688" at only one site to verify sensitivity (thin saw blades provided by NIAR)
- Simulated flaw growth (SFG) attempted to mimic forcing of plate structure without creating damage – no significant effect on damage metric
- Sensitivity observed to certain notch increases, but trend not linear
 - sensitive to first notch cut
 - significant drop after fastener installed and removed (FIR)
 - Metric grows with larger notches
- Jump observed after two week delay in testing – 'still in noise'
- Larger cuts will be applied for validation studies







Demonstration Study: Focused on Single Stage

- Phase II Laboratory Testing of Relevant Structures / Environment
- Assumption: Key SDS Factors can be Demonstrated in Single Study

Factors in Study:

- Flaw growth (notch):
 - First cut: 0.063", Second to 0.125",
 repeat 0.125" cuts to 1.00" (10 levels)
 - At two fastener locations with relief notches
- Environmental conditions: (ambient 72°F)
 - Temperature variation (32°F to 112°F)
 - Temperature gradients (<10°F)
 - Ambient noise (chamber on / off)
- Boundary conditions:
 - Loading / unloading mass on structure (10 lb)
 - Fastener removal and reinstall (75 in-lbs +/- 10 in-lbs) 'simulate maintenance'
- Sensor conditions: Evaluate accelerometer bond reinstallation (ref., second)











Measurement / POD Model







Measurement / POD Model



Fit Measurement 'Model' (Using Empirical Data)

•Flaw length (a_1): $dm = \beta_0 + \beta_1 * a_1 + \beta_2 * a_1^2 + \beta_3 * a_1^3$

•Flaw location (*a*₂)

• Evaluate both 'combined' and 'separate' flaw location scenarios fits

•Normalized mean **temperature** (a_3) , and absolute value $|a_3|$

•Normalized temperature gradients (a₄),

•Abs. difference between temp. and nearest reference (a_5)

•Ambient noise level (a_6) ,

•Sensor status (active, failed)

Level 2: Uncertainty in Model Parameter Estimate



Regression Analysis Example (R)

Code:	data.tmp <- read.csv('analy ref1 flaw3.csv',header=FALSE)
	x1 <- data.tmp\$V1
	x2 <- data.tmp\$V2
	x3 <- data.tmp\$V3
	x4 <- data.tmp\$V4
	x5 <- data.tmp\$V5
	x6 <- data.tmp\$V6
	x11 <- x1*x1
	x111 <- x1*x11
	y1 <- data.tmp\$V14
	frame1 <- data.frame(y=y1, x1=x1, x2=x2, x3=x3, x4=x4, x5=x5, x6=x6, x7 = x11, x8 =
	x111)
	$y.vs.x \le lm(formula = y \sim x1 + x2 + x3 + x4 + x5 + x6 + x7 + x8, data=frame1)$
	summary(y.vs.x)
Call:	$lm(formula = y \sim x1 + x2 + x3 + x4 + x5 + x6 + x7 + x8, data = frame1)$
Residuals:	Min 1Q Median 3Q Max
	-0.035835 -0.007133 0.001119 0.006437 0.026368
Coefficients:	Estimate Std. Error t value Pr(> t)
	(Intercept) 0.018921 0.003902 4.849 6.8e-06 ***
	x1 -0.081361 0.041766 -1.948 0.05526.
	x2 -0.003323 0.003465 -0.959 0.34072
	x3 0.010309 0.003690 2.794 0.00665 **
	x4 -0.009321 0.005813 -1.603 0.11315
	x5 0.032816 0.010755 3.051 0.00318 **
	x6 0.005763 0.013645 0.422 0.67402
	x7 0.373822 0.109798 3.405 0.00108 **
	x8 -0.205131 0.072407 -2.833 0.00596 **
	Signif. codes: 0 '***' 0.001 '**' 0.01 '*' 0.05 '.' 0.1 ' ' 1
	a
Diagnostics:	Residual standard error: 0.01303 on 73 degrees of freedom
-	Multiple R-squared: 0.9133, Adjusted R-squared: 0.9037
	F-statistic: 96.07 on 8 and 73 DF, p-value: < 2.2e-16
Significant	 x1 <- data.tmp\$V1: Flaw size (a1) (Part of flaw size model)
Factors:	• $x_3 \le \text{data.tmp}$ Normalized mean temperature (a_2)
	• $x5 \le data.tmp$ \$V5: Normalized temperature gradients (a_3)
	• $x^{7} \leq x^{11} \leq x^{1*}x^{1}$ Flaw size model term: $(a_{1})^{2}$
	• $x_1 \sim x_1 \sim x_1 \times x_1$ fraw size model terms $(a_1)^3$
	• $x_0 > x_{111} > x_1 x_{11}$ Flaw size model term: (a_1)



Input

Parameters









POD Results: Dependency on Flaw Location



Can Improve POD by Choosing *Optimal Sensor Configuration*:



POD Results – Impact of Sensor Durability



POD Evaluation Must Address Known Sensor Durability Issues:

- Issue demonstrated by percent of C–17 in-service strain gauge failures as a function of time [Ware et al] ^{0.50}
 0.45
- Bathtub Curve Model [Meeker and Escobar]



Evaluation of Impact of Sensor Failure:

- Evaluate changes in POD due to random sensor failure over time
- Explore failure of two sensors (25%) over first six years of service life
- Distributions of Time to Failure Considered in Evaluation



Consequence of SHM False Calls-KC-130J Exceedances

Monitoring system:

- Sensors: Fuel Quality, Accelerometers, Differential Pressure, Discrete, Position
- 25 Parameters Measured

Consequence of Indication

- All reported KC-130J exceedances require engineering disposition due tc
- Squadron sends SHM download files
- Aircraft Structural Life Surveillance engineers assess data/provide recommendation to Fleet Support Team (FST) [engineering costs]
- FCs result in unnecessary inspections, affect aircraft availability





POD Results – Impact of Sensor Durability



 Sensor Scenarios with Corresponding Changes in POD and False Call Rate:

Approach 1: (Best Sensitivity) - Use accel. #1 as reference - Use accel. #6 as source



Scenarios Addressing Sensor Failure



- Use median of active sensors



Approach 3: (Accel.#1 Failure) - Use accel. #8 as reference

- Use median of active sensors



Approach 4: (Accel.#8 Failure)

- Use accel. #3 as reference - Use median of active sensors





POD Results – Impact of Sensor Durability



Evaluation of Impact of Sensor Failure:

- Evaluate changes in POD due to random sensor failures over time
- Distributions of Time to Failure Considered in Evaluation
- Results: Mean expected POD and POFC at a flaw size of 1.0 in as a function of time







Summary of 'Best Practices' for NDE / SHM Characterization



- Characterization error analysis should follow standard practice for POD evaluation [e.g. MIL-HDBK 1823A]
 - Must understand implicit statistical assumptions in regression analysis [Annis et al., 2015]
 - If assumptions are not met, *pick a different 'correct' model!*
- Protocol presented for SHM capability evaluation
 - Thorough factor evaluation is critical for proper assessment [environment, varying structure, sensor and damage state]
- Demonstrated 'need' for representative models in SHM capability evaluation [empirical and/or numerical]
 - Certain flaw locations will require separate POD models [global SHM]
 - Feasible to evaluate impact of sensor failures on performance
 - Must address varying conditions and model uncertainty (error)





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